



# Applied CFD in the Metallurgical Industry

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# Outline

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- ④ What is applied CFD at MEFOS
- ④ Example: Sulphur Refining of Steel
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  - Reaction model
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- ④ Validation
  - Transport Equation
  - Sulphur refining
- ④ Conclusions



# Why are MEFOS modelling metallurgical processes?

The goal for the metallurgical industry is to achieve the **material properties** needed for production of a given product. This requires **control** of the amount of:

- Alloying elements (C, Si, Mn, Cr, Al ..)
  - Other elements (S, N, H, P, Cu, Zn ..)
  - Unwanted non-metallic particles (Inclusions). Also composition and size distribution
- Continuous **measurement** and **sampling** for **process control** is difficult in most process steps. The models are therefore needed for:
- Optimisation of the different process steps
  - Development of process control systems
  - Enhanced understanding
  - Education



# What is applied CFD at MEFOS

When fundamental models are missing or impossible to realize because of the lack of data, which is often the case, other methods need to be utilised.

One example: Fundamental data needed to describe the slag/metal-interface in a stirred ladle during sulphur refining is missing. Instead, empirical models of that interface, based on sampling at the steel plant can be used. The use is necessary if sulphur-refining in a production ladle is to be simulated.

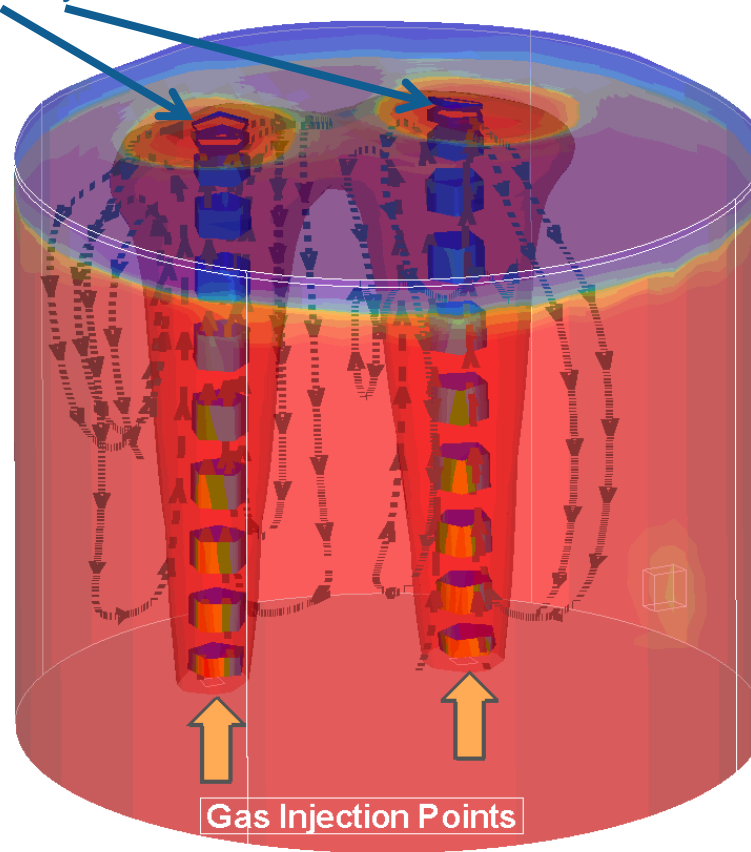




# Sulphur Refining

## Transport description (Gas Stirring)

Open eyes

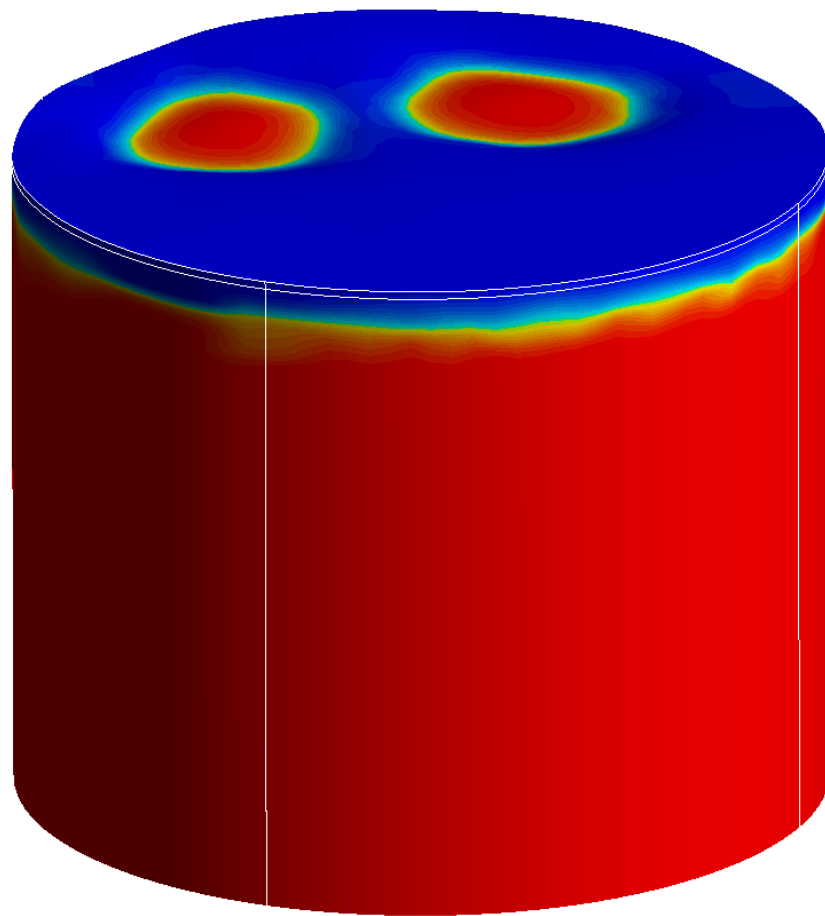


Ladle Radius = 1.25 m  
Steel Weight = 65 t  
Slag Weight = 1200 kg  
Gas Flow Rate = 100 Nl/min

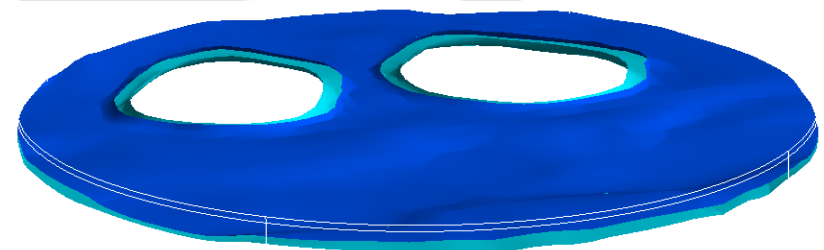


# Sulphur Refining

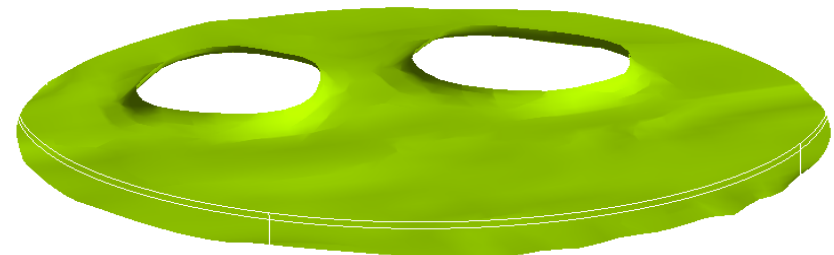
## Transport description (Gas Stirring)



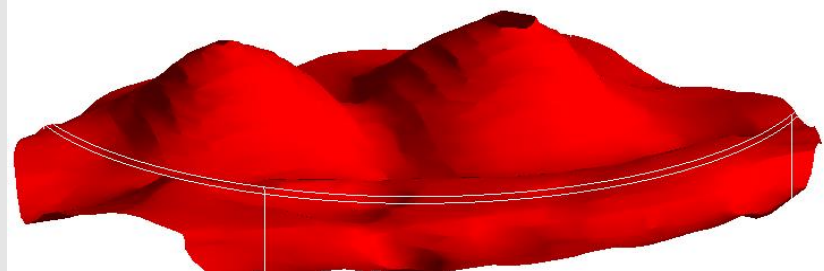
Gas Stirred Ladle



Slag Layer



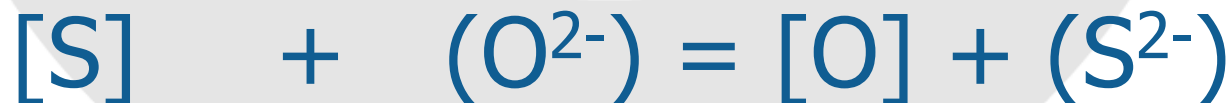
Interface (Reaction zone)



Steel Surface



# Sulphur Refining Reaction Model



5 equations 6 unknowns (Al, Fe, Mn, Si, S and O)!!!



# Sulphur Refining Reaction Model

Equation 1.  $\Delta\text{Al}$  is related to  $\Delta\text{Al}_2\text{O}_3$

Equation 2.  $\Delta\text{Fe}$  is related to  $\Delta\text{FeO}$

Equation 3.  $\Delta\text{Mn}$  is related to  $\Delta\text{MnO}$

Equation 4.  $\Delta\text{Si}$  is related to  $\Delta\text{SiO}_2$

Equation 5.  $\Delta[\text{S}]$  is related to  $\Delta(\text{S})$

$\Delta\text{O}$  is related to:

$$\Delta[\text{wt}\%\text{O}] = \Delta[\text{wt}\%\text{O}]_{\text{Al}_2\text{O}_3} + \Delta[\text{wt}\%\text{O}]_{\text{FeO}} + \Delta[\text{wt}\%\text{O}]_{\text{MnO}} + \Delta[\text{wt}\%\text{O}]_{\text{SiO}_2} + \Delta[\text{wt}\%\text{O}]_{\text{S}}$$

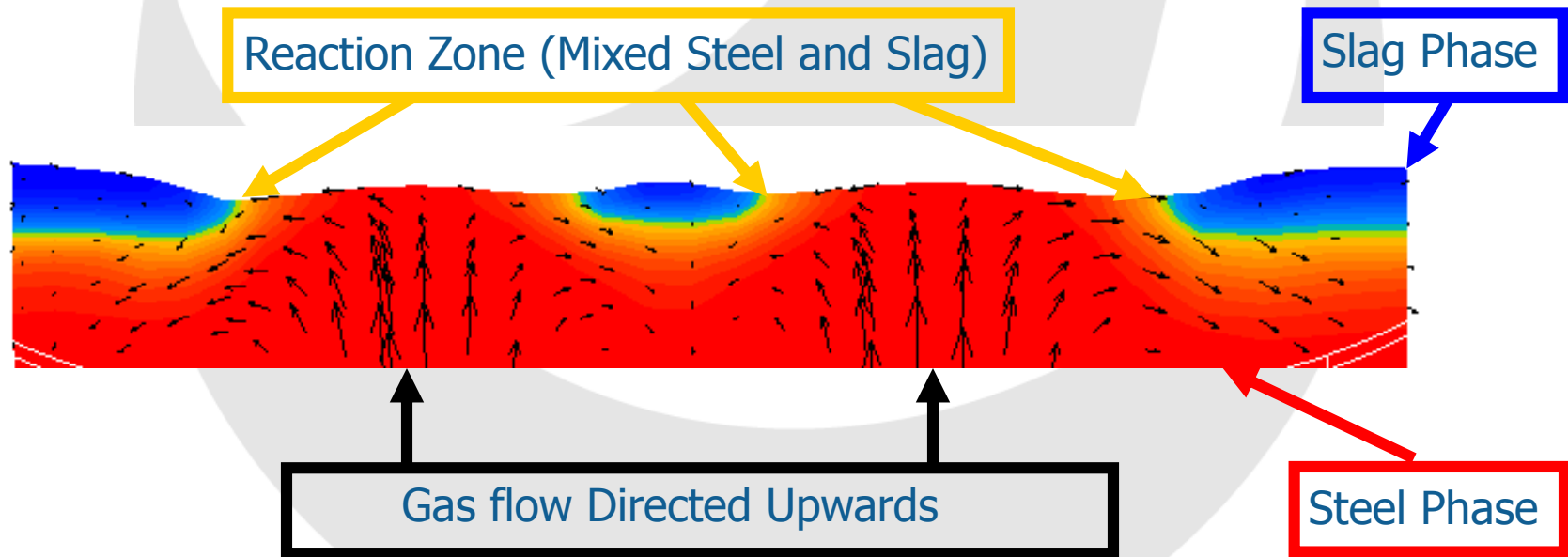




# Reaction Zone

## Scalar Equation model

Top part of a Plane in the in the ladle, through the open eyes



# Reaction Zone Sampling (Empirical model)



Sampler

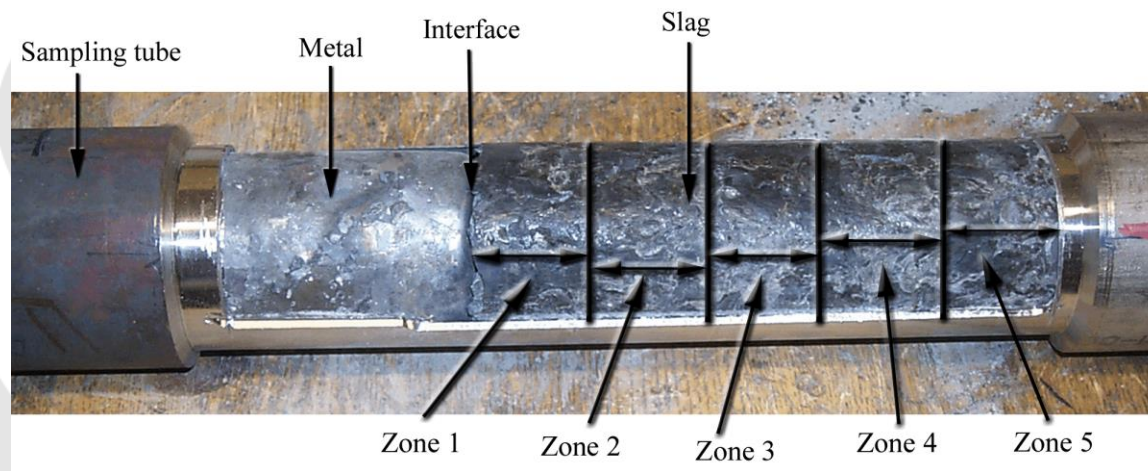


Sampling in the ladle



After sampling

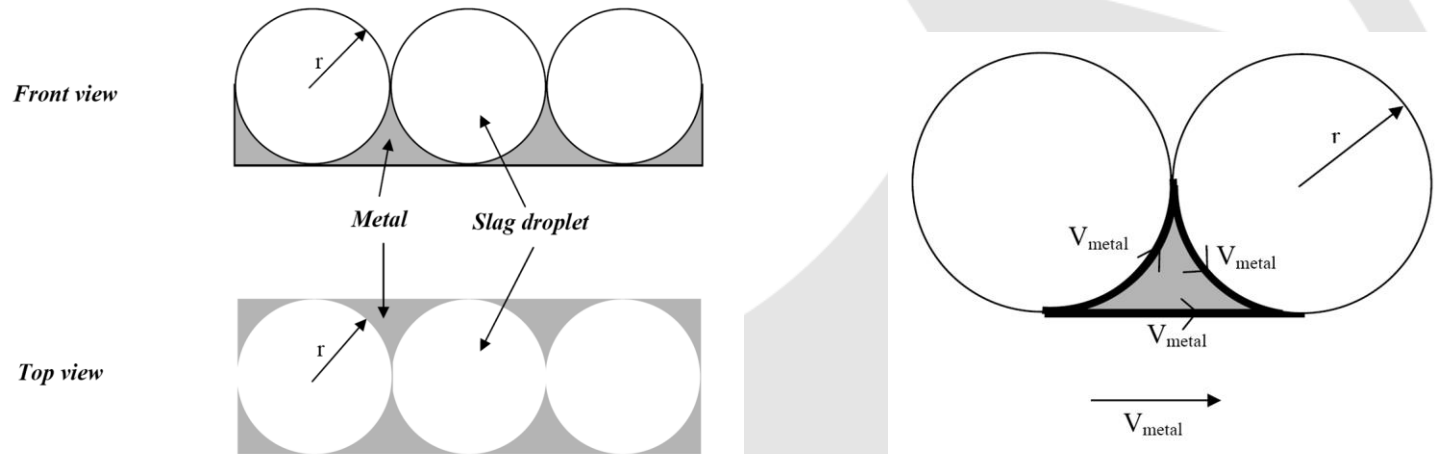
# Reaction Zone Sampling (Empirical model)



After sampling and quenching, each sample was mechanically opened. The metal bulk, slag bulk and slag-metal interface can be easily identified. Thereafter, the slag part was physically divided into a number of zones on the basis of the distance from the slag-metal interface. The width of each zone was not constant for all the samples. Small pieces of collected slag were analyzed using light optical microscope (LOM) and scanning electron microscope (SEM). The chemical compositions of the slag samples were analyzed and the sulphur contents were determined.



# Reaction Zone Empirical Model



The figures shows schematically the contact of metal with the lowest layer of slag droplets and the flow of metal associated with slag droplets. The following assumptions are made:

1. After stabilization of the flow, the whole slag layer is in droplet form.
2. All slag droplets are spherical and having the same size and shape.
3. The linear velocity of the metal along the periphery of the slag droplet is equal to the velocity of the bulk flow of the metal at the slag-metal interface.
4. The contribution of the metal film covering each slag droplet to the rate of mass exchange is negligible.



# Reaction Zone

## Empirical Model

The metal volume associated with each slag droplet can be expressed by:

$$v = \frac{1}{2} \left[ (2r)^3 - \frac{4}{3} \pi r^3 \right] \quad (1)$$

The mass of the metal associated with all slag droplets is given by:

$$M_{total\_cell} = \frac{1}{2} \left[ (2r)^3 - \frac{4}{3} \pi r^3 \right] \left( \frac{a^2}{4r^2} \right) \rho_m \quad (2)$$

The average time to travel a distance of 2 r can be evaluated by

$$t_{av} = \frac{1}{2} \left( \frac{\pi r}{V_{metal}} + \frac{2r}{V_{metal}} \right) \quad (3)$$

The time required to flush out all the metal can be written as

$$t_{flush} = t_{av} = \frac{1}{2} \left( \frac{\pi r}{V_{metal}} + \frac{2r}{V_{metal}} \right) \quad (4)$$

The flush-out rate of the metal in a unit cell can be expressed by:

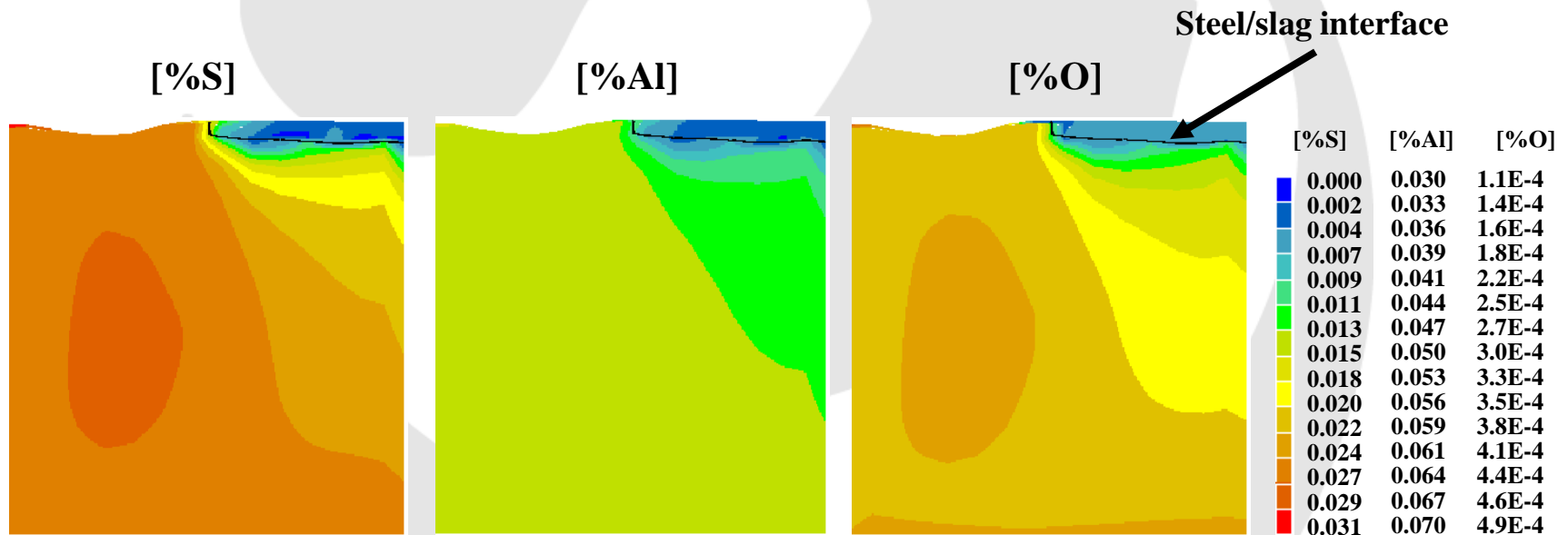
$$K_{metal} = \frac{M_{total\_cell}}{t_{flush}} \quad (5)$$

Eqs. (2) to (5) lead to

$$K_{metal} = 0.185 \rho_m V_{metal} a^2 \quad (6)$$



# Sulphur Refining and Reoxidation Model





# Validation

## Transport description

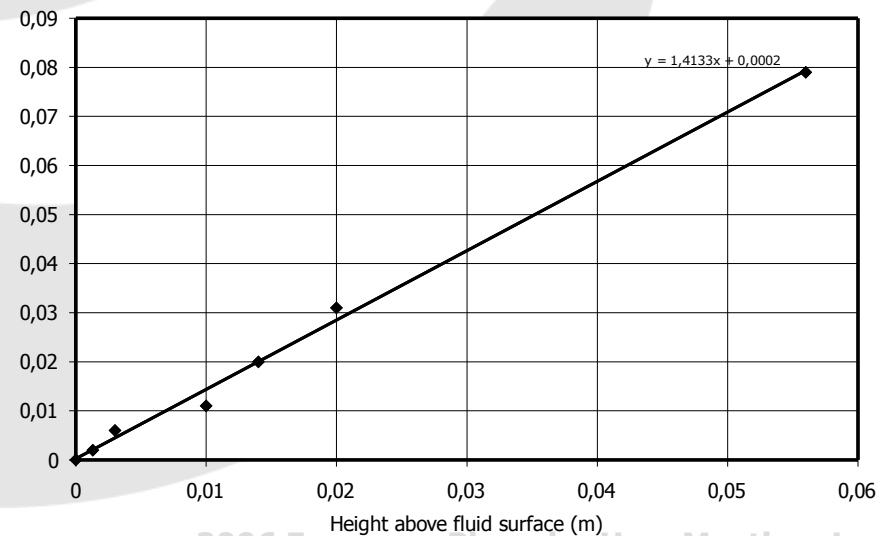
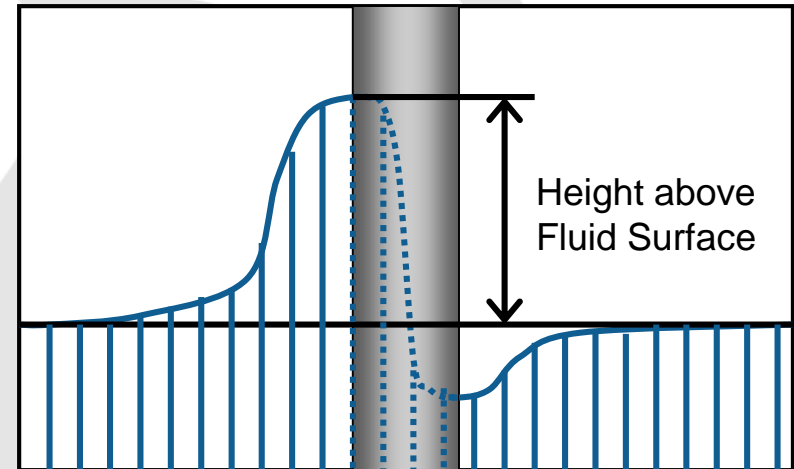
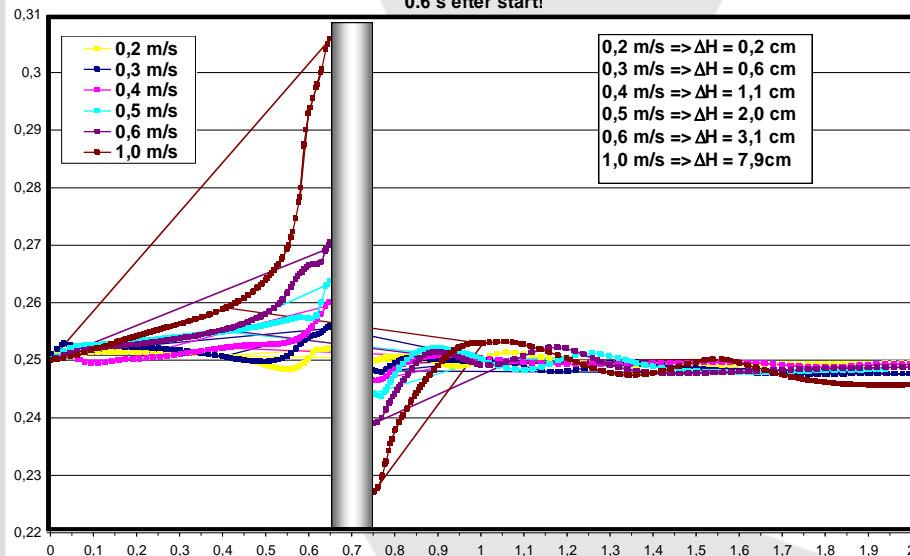
Velocity measurements with graphite rods



# Validation Wave Height Model

## Simulated waveheight

0.6 s after start!





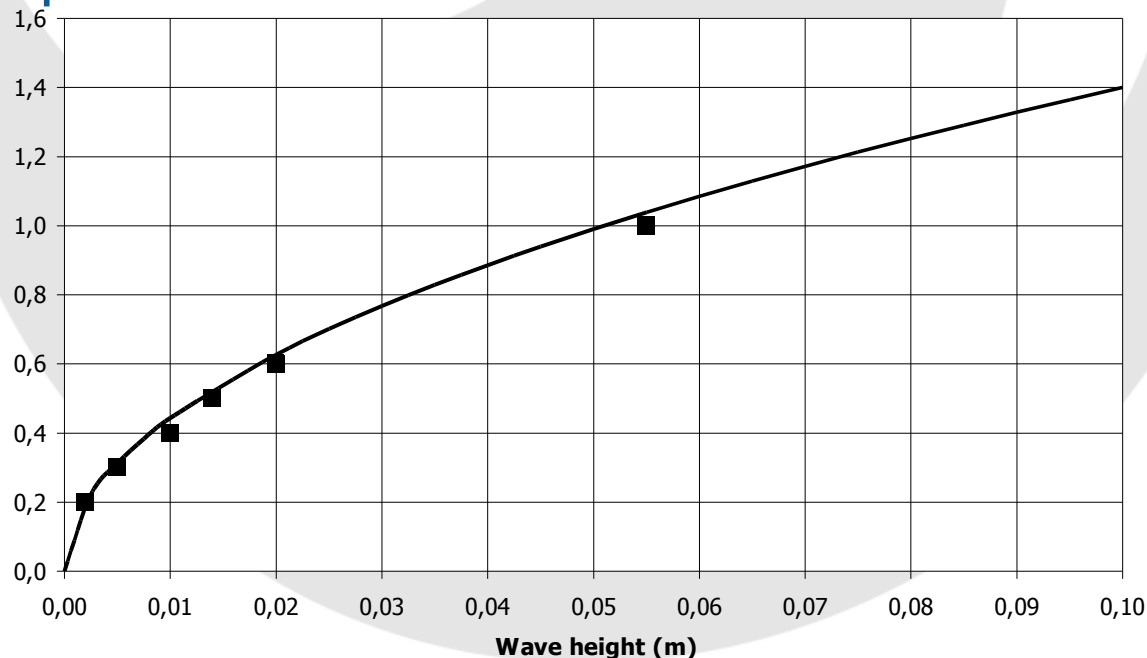
# Validation

## Validation of Wave Height Model

Bernoulli's equation for incompressible flow

$$\frac{v^2}{2} + gh + \frac{p}{\rho} = \text{Constant} \Rightarrow v_0^2 = 2gh_1 \Rightarrow v_0 = \sqrt{2gh_1}$$

Comparison between Bernoulli and simulation



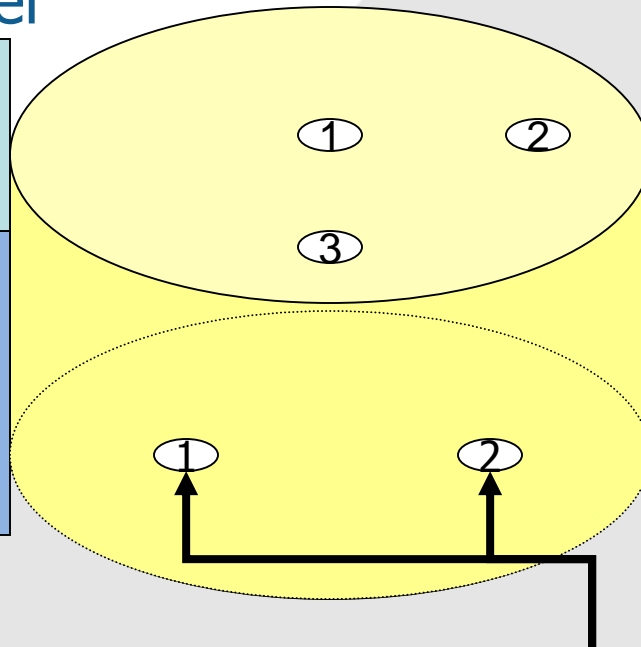
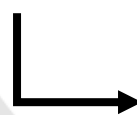


# Validation

## Transport Description

Measuring positions in the ladle

Induction stirrer



Porous plugs for gas injection





# Validation Transport Description

Velocity measurements with graphite rods

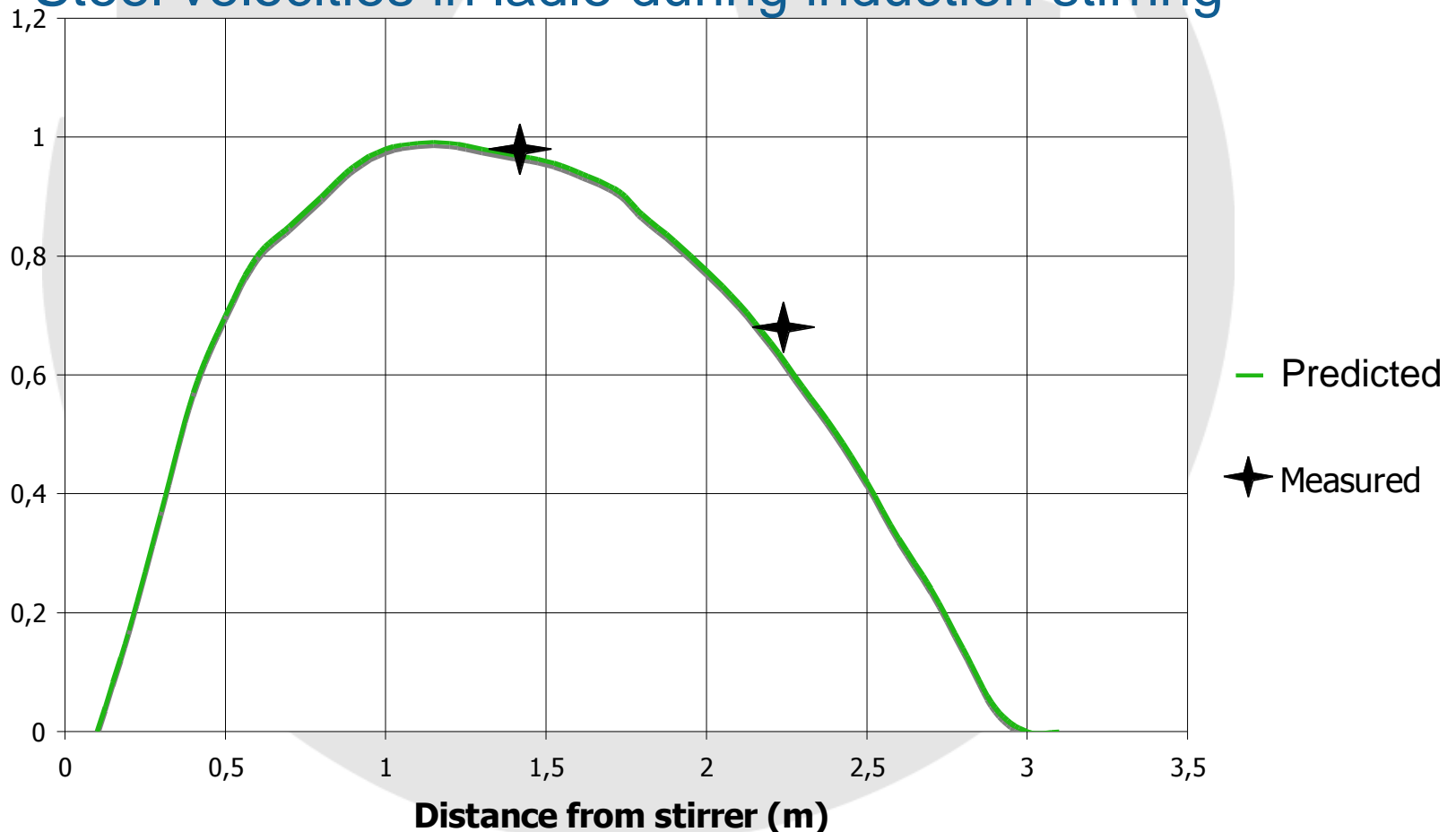




# Validation

## Transport Description

Steel velocities in ladle during induction stirring







# Validation

## Sulphur Refining and Reoxidation

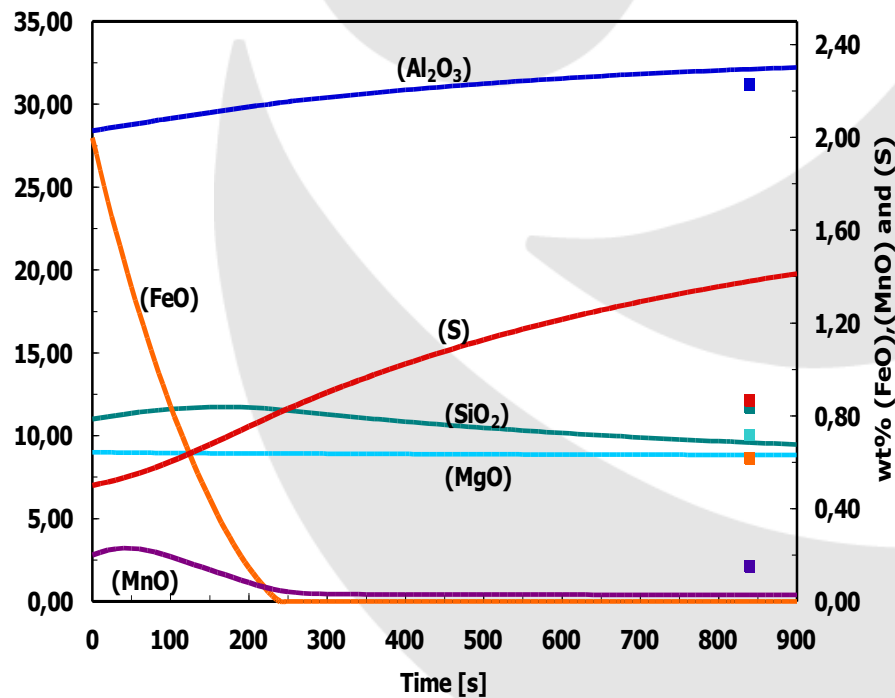
For a validation of the "Sulphur refining and reoxidation predictions from the model a comparison between predicted results and data from the industry was performed. Slag and Steel was sampled before and after the sulphur refining process. The process took 850 seconds and was performed in vacuum making it impossible to sample during the process. The two sets of Slag and Steel samples were analysed and used as input data and resulting Steel analysis respectively.



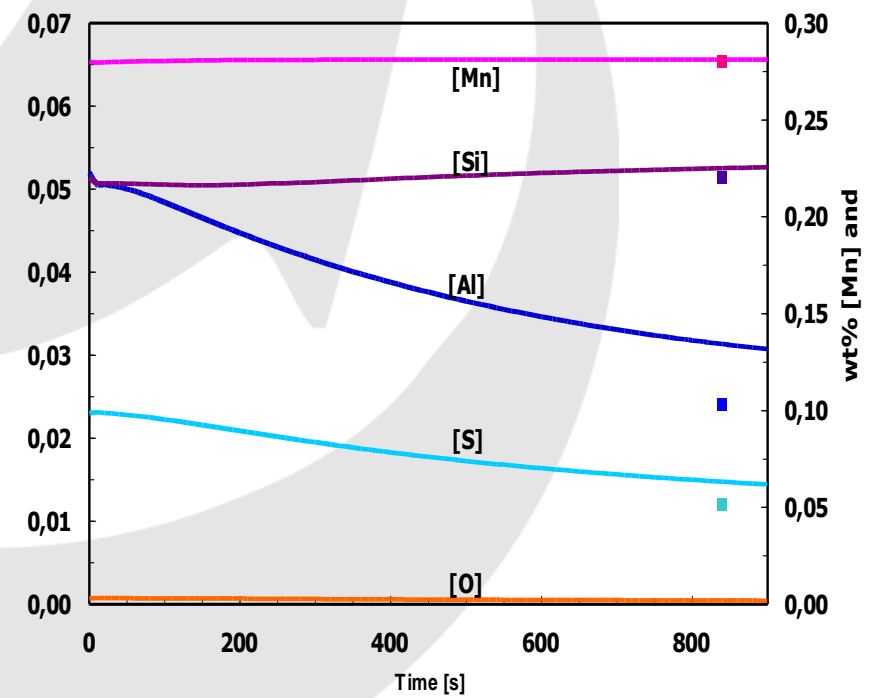
# Validation

## Sulphur Refining and Reoxidation

Slag analysis



Steel analysis



■ Measured

— Predicted



# Conclusions

- For a Qualitative description (Parametric studies) a simpler reaction zone model can be used.
- For a Quantitative description of Sulphur refining, the development of empirical models describing the reaction zone in a steel ladle must be utilised due to the lack of data prohibiting development of a fundamental model.